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ORNL-2896 UC-4 - Chemistry-General

# PHASE EQUILIBRIA IN MOLTEN SALT

BREEDER REACTOR FUELS.

I. THE SYSTEM LIF-BeF2-UF4-ThF4

C. F. Weaver R. E. Thoma H. Insley H. A. Friedman



# OAK RIDGE NATIONAL LABORATORY

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ORNL-2896 UC-4 - Chemistry-General TID-4500 (15th ed.)

Contract No. W-7405-eng-26

#### REACTOR CHEMISTRY DIVISION

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#### PHASE EQUILIBRIA IN MOLTEN SALT BREEDER REACTOR FUELS. I. THE SYSTEM LiF-BeF<sub>2</sub>-UF<sub>4</sub>-ThF<sub>4</sub>

C. F. Weaver R. E. Thoma H. Insley H. A. Friedman

#### ABSTRACT

The phase equilibrium relationships for the systems limiting the quaternary system LiF-BeF<sub>2</sub>-UF<sub>4</sub>-ThF<sub>4</sub> are described in detail along with available information on the quaternary system itself. The implications of the extensive solid solutions in the limiting systems are discussed and experimental information supporting the conclusions is presented. The optical properties, crystallographic properties, and x-ray diffraction patterns for the phases occurring in these systems are tabulated. Specific compositions of project interest to which references have been made in the ORNL literature are given special attention. Reference is made to literature reporting properties of these materials other than those discussed in this report.

#### 1. INTRODUCTION

Fluoride fused salts have attracted general interest for use in hightemperature reactors because: (1) fluorine has a very low thermal neutron absorption cross section,<sup>1</sup> (2) fluorides have low vapor pressures at temperatures and compositions of interest,<sup>2</sup> (3) molten fluorides are very resistant to damage by nuclear emissions,<sup>2</sup> and (4) there are no serious corrosion problems between many fluorides and nickel-based structural material.<sup>2</sup> Specifically, uranium tetrafluoride, a fissile material, is of interest because it is the only nongaseous fluoride of uranium which does not incur serious metal container corrosion and/or fuel inhomogeneity as an effect of high-temperature disproportionation.<sup>3</sup> Thorium tetrafluoride,

<sup>1</sup>S. Glasstone, <u>Principles of Nuclear Reactor Engineering</u>, p 841, Van Nostrand, Princeton, N.J., 1955.

<sup>2</sup>H. G. MacPherson, p 567 in Fluid Fuel Reactors, ed. by J. A. Lane,
H. G. MacPherson, and F. Maslan, Addison-Wesley, Reading, Mass., 1958.
<sup>3</sup>W. R. Grimes et al., p 577 in Fluid Fuel Reactors, ed. by J. A.
Lane, H. G. MacPherson, and F. Maslan, Addison-Wesley, Reading, Mass., 1958.

a fertile material, is the only fluoride of thorium.<sup>4</sup> The fluorides  $PbF_2$ , BiF<sub>3</sub>, Li<sup>7</sup>F, NaF, ZrF<sub>4</sub>, and BeF<sub>2</sub> have sufficiently low thermal neutron absorption cross sections, vapor pressures, and melting points to allow their use as diluents for the UF<sub>4</sub> and ThF<sub>4</sub>. However,  $PbF_2$  and BiF<sub>3</sub> are unsuitable because the cations are readily reduced to the metallic state by structural metals such as iron and chromium.<sup>5</sup> The lower thermal neutron absorption cross section of Li<sup>7</sup> as compared with that of sodium allows the design of reactors which have a smaller holdup of fissile material and superior breeding performance.<sup>6</sup>

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Fluid salt mixtures containing high concentrations of  $ZrF_4$  are not regarded as attractive reactor fluids because of significant vapor pressure of  $ZrF_{4}$  above 500°C. In a reactor system sublimation of  $ZrF_{4}$  followed by deposition as a solid limits the temperatures at which long operating times are permissible. Comparable limitations do not occur in mixtures containing BeF<sub>2</sub> rather than  $ZrF_4$ .<sup>7</sup> Molten salt reactor systems which are designed to operate at sufficiently high temperatures that alkali fluoride-ZrF4 solvents containing 30-40 mole % ZrF4 can be employed may offer advantages in the future, but present preference must be given to BeF<sub>2</sub> on the basis of sublimation.<sup>8</sup> Consequently, mixtures containing Li<sup>7</sup>F, BeF<sub>2</sub>, UF<sub>4</sub>, and ThF<sub>4</sub> which have liquidus values several hundred degrees below the  $ThF_4$  and  $UF_4$  melting points are the most promising core materials for a fused salt thermal breeder/converter reactor. A knowledge of the liquidus values of such mixtures is necessary since as reactor fluids they must remain wholly in the liquid state during reactor operation. Liquidus data alone are insufficient because mixtures of solids and liquids will be formed during some fuel handling operations. A knowledge of the nature of the melting-freezing process, of the uranium-thorium partition or phase separation during this process, and of the identity of

<sup>4</sup><u>Toid</u>., p 588. <sup>5</sup><u>Tbid</u>., p 570.

<sup>6</sup>MSR Quar. Prog. Rep. Jan. 31, 1958, ORNL-2474, p 1.

<sup>7</sup>H. G. MacPherson, ORNL, personal communication.

<sup>8</sup>W. R. Grimes <u>et al.</u>, p 582-84 in <u>Fluid Fuel Reactors</u>, ed. by J. A. Lane, H. G. MacPherson, and F. Maslan, Addison-Wesley, Reading, Mass., 1958.

solids formed on cooling of molten mixtures is also necessary. Thus, the phase equilibrium relationships for the quaternary system must be understood, especially near liquidus temperatures and at compositions which may afford attractive core or blanket materials. Before the determinations of the phase relationships can be made in a quaternary system, the 14 limiting unary, binary, and ternary systems must be understood. All these limiting systems for the quaternary system LiF-BeF<sub>2</sub>-UF<sub>4</sub>-ThF<sub>4</sub> have been reported and are described in detail in the body of this report along with the available data on the quaternary system itself. It is remarkable that these studies have not disclosed the existence of ternary or of quaternary compounds.

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The majority of the information included in this report was derived in the High Temperature Phase Equilibrium Group of the Reactor Chemistry Division at the Oak Ridge National Laboratory. Some of the preliminary studies of the phase equilibria in the limiting binary and ternary systems were begun as early as 1951.

#### 2. EXPERIMENTAL METHODS

#### 2.1 Techniques and Apparatus

The experimental techniques and apparatus used in the studies of  $LiF-BeF_2-UF_4-ThF_4$  phase equilibria have been described in detail elsewhere.<sup>9-13</sup> In general, the data were obtained by thermal analysis of slowly cooled melts and by quenching mixtures which had been equilibrated at known temperatures. Commonly, fused-salt diagrams are based entirely on information from cooling curves (temperature of the sample plotted as a function of time). Changes in the slope of the cooling curve reflect phase changes which occur on cooling, but are prone to give misleading or irrelevant indications because of the impossibility of maintaining equilibrium during the cooling process. Consequently, predominant use

<sup>&</sup>lt;sup>9</sup>C. J. Barton et al., J. Am. Ceram. Soc. <u>41</u>, 63-69 (1958).

<sup>&</sup>lt;sup>10</sup>C. J. Barton et al., J. Phys. Chem. <u>62</u>, <u>66</u>5 (1958).

<sup>&</sup>lt;sup>11</sup>H. A. Friedman, J. Am. Ceram. Soc. 42, 284-85 (1959).

<sup>&</sup>lt;sup>12</sup>P. A. Tucker and E. F. Joy, Am. Ceram. Soc. Bull. <u>36</u>, 52-54 (1957). <sup>13</sup>L. J. Wittenberg, J. Am. Ceram. Soc. <u>42</u>, 209-11 (1959).

has been made of the much more effective method of quenching equilibrium samples and identifying the phases by examination with a polarizing light microscope and by x-ray diffraction techniques.

A thermal gradient furnace with a single moving thermocouple<sup>11</sup> is used for equilibration in the temperature range 650-1200°C. Five other thermal gradient furnaces, operating at a maximum temperature of 900°C, incorporate 18 thermocouples each. The independent readings from these are used to determine a temperature calibration curve of the thermal gradient within the annealing area of the furnace. Malfunction of a single thermocouple becomes readily apparent. In quenching studies made at temperatures below 900°C, sample tubes are distributed among the five furnaces randomly, to achieve maximum reproducibility among independent temperature readings. The region of temperature overlap, 650-900°C, is used to monitor the single high-temperature furnace. In the absence of supercooling effects, the completely separate measurements in the thermal analysis furnaces agree within 5°C with those from the thermal gradient furnaces. This interlocking system, by which multiple thermocouples within five of the furnaces and three types of furnaces are used, provides a continuous check on the proper function of the equipment.

The accuracy of the temperature measurements is limited by the characteristics of the Chromel-Alumel thermocouples used.<sup>14</sup> The invariant point temperature data are so precise that a standard deviation of 1 or 2° is obtained.

#### 2.2 Materials

The LiF used for this work was reagent grade obtained from Foote Mineral Company and from Maywood Chemical Works. The UF<sub>4</sub> was a product of Mallinckrodt Chemical Works. The ThF<sub>4</sub> was obtained from Iowa State College and from National Lead Company. The BeF<sub>2</sub> was a product of Brush Beryllium Company. No impurities were found in any of these materials by x-ray diffraction or microscopic analysis. Spectroscopic analysis indicates less than 0.25 wt % impurities.

<sup>14</sup>J. F. Potts, <u>Thermocouple Research - Cold Work</u>, ORNL CF-59-6-61 (June 15, 1959).

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Because thorium<sup>15</sup> and uranium fluorides are easily converted to oxides or oxyfluorides at elevated temperatures it was necessary to remove small amounts of water and oxygen as completely as possible from the starting materials. In a few cases the molten mixtures were treated with anhydrous HF. For the vast majority of preparations, however, NH<sub>2</sub>F·HF was added to the mixture before melting. As such mixtures are heated the water evaporates from the system. Trace quantities of oxide impurities are converted to products which have not yet been identified but which are likely to be ammonium "fluometallates."16,17 Upon further heating the ammonium "fluometallates" and the excess NH4F.HF decompose. The products are metal fluorides and the gases  $NH_3$  and HF. These gases are quantitatively swept from the system by dry helium. The samples were melted and cooled to obtain thermal analysis data. The purified solids were transferred to an argon-filled dry box which contained BaO as a desiccant. They were ground to pass a 100-mesh screen and used in the quenching experiments. The heating cycles were conducted in closed capsules or under an atmosphere of dry helium or argon.

#### 3. PHASE EQUILIBRIA AND RELATED PHENOMENA

3.1 The Components LiF, BeF2, ThF4, and UF4

A special character can be assigned to the behavior of combinations of the four compounds LiF,  $BeF_2$ ,  $ThF_4$ , and  $UF_4$ , for in this grouping are to be found a pair of metal cations in the lowest and a pair in the highest atomic number range. It might, therefore, be expected that the diverse physical and chemical properties of these four components would contribute to the occurrence of phase behavior in which a wide variety of phenomena would appear. The melting points of the components are shown in Table 1.

Of the four components, only  $BeF_2$  exhibits polymorphic transitions. The equilibrium melting temperature and the nature of these solid-state

<sup>&</sup>lt;sup>15</sup>R. W. M. D'Eye, J. Chem. Soc. 1958, 196.

<sup>&</sup>lt;sup>16</sup>MSR Quar. Prog. Rep. Apr. 30, <u>1959</u>, ORNL-2723, p 93.

<sup>&</sup>lt;sup>17</sup>B. J. Sturm, ORNL, personal communication (May 1960).

Table 1. The Melting Points of the Components

· · · · · · · · · · · · · · · · · · ·	· . ·	Component	Melting Point (°C)	
	·.	LiF	845 <sup>ª</sup>	· · · · · · · · · · · · · · · · · · ·
		BeF <sub>2</sub>	548 <sup>b—d</sup>	
		ThF <sub>4</sub>	ıııı <sup>e-g</sup>	· · ·
· · ·	· ·	UF <sub>4</sub>	1035 <sup>h</sup>	• •

<sup>a</sup>T. B. Douglas and J. L. Dever, J. Am. Chem. Soc. <u>76</u>, 4824 (1954). <sup>b</sup>R. E. Thoma <u>et al.</u>, "Phase Equilibria in the Systems BeF<sub>2</sub>-ThF<sub>4</sub> and LiF-BeF<sub>2</sub>-ThF<sub>4</sub>," J. Phys. Chem., in press.

D. M. Roy, R. Roy, and E. F. Osborn, J. Am. Ceram. Soc. <u>36</u>, 185 (1953).

<sup>d</sup>M. P. Boryenkova et al., Zhur. Neorg. Khim. <u>1</u>, 2071 (1956).

<sup>e</sup>R. E. Thoma et al., J. Phys. Chem. <u>63</u>, 1266 (1959).

<sup>f</sup>J. Asker, E. R. Segnit, and A. W. Wylie, J. Chem. Soc. <u>1952</u>, 4470. <sup>g</sup>A. J. Darnell and F. J. Keneshea, Jr., J. Phys. Chem. <u>62</u>, 1143 (1958).

<sup>n</sup>H. R. Hoekstra and J. J. Katz, p 177 in <u>The Actinide Elements</u>, ed. by G. T. Seaborg and J. J. Katz, McGraw-Hill, <u>New York</u>, 1954.

transitions have been the subject of controversy for several years.<sup>18</sup> The structure of  $BeF_2$  is analogous to that of  $SiO_2$ , as was predicted by Goldschmidt;<sup>19</sup> all known modifications crystallize as  $SiO_2$ -type structures. Being similar to  $SiO_2$ ,  $BeF_2$  readily forms a glass upon cooling from the liquid state. For this reason, establishing solid-state equilibria with  $BeF_2$ , in which devitrification of this glass must be accomplished, is often a very slow process.

Optical and crystallographic properties for the compounds LiF,  $BeF_2$ ,  $ThF_4$ , and  $UF_4$  may be found in Appendix A. Their x-ray diffraction data are listed in Appendix B.

<sup>18</sup>A. V. Novoselova, Uspekhi Khim. 27, 33 (1959).
<sup>19</sup>V. M. Goldschmidt, Skrifter Norske Videnskaps-Akad. Oslo. I.
Mat.-Naturv. Kl. 1926, No. 8, p 7-156 (1927).

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The systems  $BeF_2$ -Th $F_4^{20}$  (Fig. 1) and  $BeF_2$ -UF $_4^{21}$  (Fig. 2) are similar



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Fig. 2. The System BeF<sub>2</sub>-UF<sub>4</sub>.

liquidus slope in the quadrivalent fluoride primary phase region. The eutectic invariant points are at 2 mole % ThF<sub>4</sub>, 527°, and at 0.5 mole % UF<sub>4</sub>, 535°, while the change in slope occurs near 12 mole % ThF<sub>4</sub> and 7 mole % UF<sub>4</sub> in the corresponding systems.

#### 3.3 The System LiF-BeF<sub>2</sub>

A phase diagram of the system  $\text{LiF-BeF}_2^{22,23}$  (Fig. 3) has been derived at ORNL from the results of thermal gradient experiments. A phase diagram nearly identical with that shown has been derived independently at the

<sup>22</sup>R. E. Thoma (ed.), Phase Diagrams of Nuclear Reactor Materials, ORNL-2548, p 33 (Nov. 2, 1959).

<sup>23</sup>R. E. Moore, C. J. Barton, R. E. Thoma, and T. N. McVay, ORNL, unpublished data.



Fig. 3. The System LiF-BeF<sub>2</sub>.

Mound Laboratory.<sup>24</sup> These diagrams are revisions of those published by earlier investigators.<sup>25-27</sup> Two equilibrium compounds occur in the system LiF-BeF<sub>2</sub>, the incongruently melting compound 2LiF.BeF<sub>2</sub> and the subsolidus compound LiF.BeF2. Unsuccessful attempts have been made by the authors to produce the reported compounds 3LiF.2BeF2<sup>28</sup> and LiF.2BeF2<sup>25</sup> by devitrification of LiF-BeF<sub>2</sub> glass and by solid-state equilibration of mixtures of BeF, and 2LiF.BeF,. Because the special purification techniques described earlier in this report were not used by other investigators<sup>25,28</sup> reports of the existence of 3LiF.2BeF2 and LiF.2BeF2 should be considered tentative.

The optical properties, crystallographic properties, and x-ray diffraction data for the compounds 2LiF.BeF2 and LiF.BeF2 are listed in Appendixes A and B. The compositions and temperatures of the two invariant points and one upper limit of stability may be found in Table 2.

Mole % BeF <sub>2</sub> in Liquid	Invariant Temperature (°C)	Type of Equilibrium	Phase Reaction at Invariant Temperature
33.5	454	Peritectic	$L + LiF \rightleftharpoons 2LiF \cdot BeF_2$
52	355	Eutectic	$L \rightleftharpoons 2LiF \cdot BeF_2 + BeF_2$
-	280	Upper temperature of stability for LiF•BeF <sub>2</sub>	$2 \text{LiF} \cdot \text{BeF}_2 + \text{BeF}_2 \rightleftharpoons \text{LiF} \cdot \text{BeF}_2$

Table 2. Invariant Equilibria in the System LiF-BeF2\*

\*R. E. Thoma (ed.), Phase Diagrams of Nuclear Reactor Materials, ORNL-2548, p 33 (Nov. 6, 1959).

Cooling mixtures of LiF and BeF<sub>2</sub> slowly from the liquid to the solid state rarely produces equilibrium solids, for the subsolidus reaction

<sup>24</sup>J. F. Eichelberger, C. R. Hudgens, L. V. Jones, and T. B. Rhinehammer, Mound Laboratory, unpublished data.

<sup>25</sup>D. M. Roy et al., J. Am. Ceram. Soc. <u>37</u>, 300 (1954).
 <sup>26</sup>A. V. Novoselova et al., J. Phys. Chem. (USSR) <u>26</u>, 1244 (1952).
 <sup>27</sup>J. L. Speirs, Ph.D. thesis, University of Michigan, May 29, 1952.

<sup>28</sup>E. Thilo and H. A. Lehmann, Z. anorg. Chem. <u>258</u>, 332-55 (1949); Ceram. Abstr. 1950, 82f.

 $\text{Li}_2\text{BeF}_4 + \text{BeF}_2 \rightarrow 2\text{LiBeF}_3$  proceeds very slowly. The compound  $\text{LiF}\cdot\text{BeF}_2$ may be observed to grow slowly into solid mixtures of LiF and  $\text{BeF}_2$  which are held for several days at temperatures just below 280°C. The formation of LiF-BeF<sub>2</sub> glass which devitrifies slowly also prevents compositions rich in BeF<sub>2</sub> from reaching equilibrium rapidly. Mixtures of LiF and BeF<sub>2</sub> containing more than 33.3 mole % BeF<sub>2</sub> regularly contain only 2LiF·BeF<sub>2</sub> and the low-quartz form of BeF<sub>2</sub> if they are cooled under nonequilibrium conditions.<sup>29,30</sup>

The compositions, liquidus temperatures, and primary phases for mixtures of LiF and  $BeF_2$  which have been referred to in the ORNL literature as C-74, C-112, and C-132 may be found in Appendix C.

Solubilities of NaF,<sup>31</sup> RbF,<sup>32</sup> ZrF<sub>4</sub>,<sup>33</sup> PuF<sub>3</sub>,<sup>34</sup> CeF<sub>3</sub>,<sup>35</sup> HF,<sup>36</sup> and the noble gases<sup>37</sup> in LiF-BeF<sub>2</sub> solvents have been reported. The reactions M + HF (M = Fe, Cr, or Ni),<sup>38</sup> CeF<sub>3</sub> + BeO,<sup>39</sup> and CeF<sub>3</sub> + H<sub>2</sub>O<sup>40</sup> in LiF-BeF<sub>2</sub> solvents have been investigated, as have the exchange reactions between CeF<sub>3</sub> and CeO<sub>2</sub> and between HfC and HfF<sub>4</sub>.<sup>41</sup>

<sup>29</sup> R. E. Thoma, <u>X-Ray Diffraction Results</u> , ORNL CF-56-6-25, item T-
<sup>30</sup> R. E. Thoma, Results of X-Ray Diffraction Phase Analyses of Fused
Salt Mixtures, ORNL CF-58-2-59, item 1894 (Feb. 18, 1958).
<sup>31</sup> R. E. Thoma (ed.), <u>Phase Diagrams of Nuclear Reactor Materials</u> , ORNL-2548, p 42 (Nov. 2, 1959). <sup>32</sup> Ibid., p 44.
<sup>33</sup> MSR Quar. Prog. Rep. Jan. 31 and Apr. 30, 1960, ORNL-2973, p 65.
ORNL-2931, p 12. <sup>35</sup> W. T. Ward, R. A. Strehlow, and G. M. Watson, Chem. Ann. Prog. Rep.
June 20, 1958, ORNL-2584, p 82.
<sup>36</sup> J. H. Shaffer and G. M. Watson, <u>Reactor Chem. Ann. Prog. Rep. Jan.</u> <u>31, 1960</u> , ORNL-2931, p 31.
<sup>37</sup> N. V. Smith <u>et al.</u> , <u>Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960</u> , ORNL-2931, p 28. <sup>38</sup> C. M. Blood et al., <u>Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960</u> .
ORNL-2931, p 39.
<sup>39</sup> J. H. Shaffer, G. M. Watson, and W. R. Grimes, <u>Reactor Chem. Ann</u> . <u>Prog. Rep. Jan. 31, 1960</u> , ORNL-2931, p 86.
<sup>40</sup> Ibid., p 88. <sup>41</sup> J. H. Shaffer and G. M. Watson, Reactor Chem. Ann. Prog. Rep. Jan.
<u>31, 1960</u> , ORNL-2931, p 82-84.

#### 3.4 The System LiF-ThF<sub>4</sub>

One congruently melting compound ( $3\text{LiF}\cdot\text{ThF}_4$ ) and three incongruently melting compounds ( $7\text{LiF}\cdot6\text{ThF}_4$ , LiF $\cdot2\text{ThF}_4$ , and LiF $\cdot4\text{ThF}_4$ ) are formed in the system LiF-ThF<sub>4</sub><sup>42</sup> (Fig. 4). Optical properties, crystallographic



properties, and x-ray diffraction data for these compounds are listed in Appendixes A and B. The compositions and temperatures of the five invariant points and one congruent melting point may be found in Table 3.

Binary LiF-ThF<sub>4</sub> mixtures containing more than 25 and less than 66.7 mole % ThF<sub>4</sub> regularly contain 3LiF.ThF<sub>4</sub> and LiF.2ThF<sub>4</sub> if cooled from the liquid state under non-

Fig. 4. The System LiF-ThF4.

equilibrium conditions.<sup>43</sup> The solidification temperature is not significantly changed by the failure of  $7\text{LiF}\cdot6\text{ThF}_4$  to form.<sup>42</sup> The equilibrium

<sup>42</sup>R. E. Thoma et al., J. Phys. Chem. <u>63</u>, 1266 (1959).

<sup>43</sup>R. E. Thoma, <u>Results of X-Ray Diffraction Phase Analyses of Fused</u> Salt Mixtures, ORNL CF-58-2-59, items 1854, 1873, and 1894 (Feb. 18, 1958).

Mole % ThF4 in Liquid	Invariant Temperature (°C)	Type of Equilibrium	Phase Reaction at Invariant Temperature
23	565	Eutectic	L ≓ LiF + 3LiF•ThF₄
25	573	Congruent mp	$L \rightleftharpoons 3LiF \cdot ThF_4$
29	568	Eutectic	$L \rightleftharpoons 3LiF \cdot ThF_4 + 7LiF \cdot 6ThF_4$
30.5	597	Peritectic	LiF·2ThF4 + L === 7LiF·6ThF4
42	762	Peritectic	$LiF \cdot 4ThF_4 + L \rightleftharpoons$ LiF \cdot 2ThF_4
58	897	Peritectic	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$

Table 3. Invariant Equilibria in the System LiF-ThF4\*

\*R. E. Thoma et al., J. Phys. Chem. 63, 1267 (1959).

condition will be readily established if the  $LiF-ThF_4$  mixtures are held for a short time at temperatures just below the solidus.

The composition, liquidus temperature, and primary phases for the mixture of LiF and  $ThF_4$  referred to in the ORNL literature as C-128 may be found in Appendix C.

#### 3.5 The System LiF-UF4

Three incongruently melting compounds (4LiF·UF<sub>4</sub>, 7LiF·6UF<sub>4</sub>, and LiF·4UF<sub>4</sub>) are formed in the system LiF-UF<sub>4</sub><sup>9</sup> (Fig. 5). The metastable





compound  $3\text{LiF} \cdot \text{UF}_4$  is readily formed from melts containing approximately 25 mole % UF<sub>4</sub> at temperatures above the incongruent melting point of  $4\text{LiF} \cdot \text{UF}_4$  when these mixtures are rapidly cooled from the liquid state. The cooling curves of samples in this composition range differ remarkably from one another depending upon the maximum temperature of the mixture just prior to cooling. The optical properties (except for  $3\text{LiF}\cdot\text{UF}_4$ ), crystallographic properties, and x-ray diffraction data for these compounds may be found in Appendixes A and B. The compositions and temperatures of the four invariant points and the lower temperature limit of stability for  $4\text{LiF}\cdot\text{UF}_4$ may be found in Table 4. The systems LiF-ThF<sub>4</sub> and LiF-UF<sub>4</sub> are similar

Mole % UF4 in Liquid	Invariant Temperature (°C)	Type of Equilibrium	Phases Present
	470	Lower stability limit for 4LiF•UF4	LiF, 4LiF•UF <sub>4</sub> , 7LiF•6UF <sub>4</sub>
26	500	Peritectic	LiF, 4LiF.UF4, liquid
27	490	Eutectic	4LiF·UF4, 7LiF·6UF4, liquid
40	610	Peritectic	7LiF·6UF4, LiF·4UF4, ilquid
57	775	Peritectic	LiF·4UF4, UF4, liquid

Table 4. Invariant Equilibria in the System LiF-UF4\*

\*C. J. Barton et al., J. Am. Ceram. Soc. 41, 63-69 (1958).

in that in each the lowest liquidus temperatures are found between 70 and 80 mole % LiF, and in both systems compounds with alkali fluoride ratios of 3:1, 7:6, and 1:4 are formed. The compounds 7LiF.6ThF<sub>4</sub> and 7LiF.6UF<sub>4</sub> form a continuous series of solid solutions as do the compounds LiF.4ThF<sub>4</sub> and LiF.4UF<sub>4</sub>. These solid solutions are described in Sec 3.10 and Appendix A.

The solubilities of NaF,<sup>44</sup> KF,<sup>45</sup> RbF,<sup>46</sup> and UF<sub>3</sub><sup>47</sup> in LiF-UF<sub>4</sub> solvents have been investigated. The vapor pressures of LiF-UF<sub>4</sub> mixtures containing 10 and 20 mole % LiF have been reported.<sup>48</sup>

<sup>44</sup>R. E. Thoma et al., J. Am. Ceram. Soc. <u>42</u>, 21-26 (1959).

<sup>45</sup>R. E. Thoma (ed.), Phase Diagrams of Nuclear Reactor Materials, ORNL-2548, p 98 (Nov. 6, 1959).

<sup>46</sup>Ibid., p 102.

47C. J. Barton et al., Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960, ORNL-2931, p 26.

<sup>48</sup>S. Langer, <u>Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960</u>, ORNL-2931, p 51.

The System UF4-ThF4 3.6



of solid solutions without maximum or minimum<sup>49</sup> (Fig. 6). The indices of refraction of the ThF4-UF4 solid solutions change regularly with composition but not linearly. The optical properties for these solid solutions may be found in Appendix A.

The System LiF-BeF2-UF4 3.7

No ternary compounds form within the system LiF-BeF<sub>2</sub>-UF<sub>4</sub><sup>50,51</sup> (Figs. 7 and 8). Consequently, the solid phases occurring in the system are those of the components or binary compounds described above (Secs 3.1, 3.2, 3.3, and 3.5). The compositions and temperatures of the five invariant points may be found in Table 5. The equilibrium phase behavior of selected compositions of LiF-BeF2-UF4 is given in Table 6 and in Appendix C. When mixtures of LiF, BeF2, and UF4 cool slowly from the liquid state, equilibrium is rarely, if ever, achieved. In the compositions C-75, C-126, C-130, C-131, and C-136 solids have been routinely observed in the cooled melts which are indicative of nonequilibrium cooling.52-54

$^{49}$ C. F. Weaver et al., Phase Equilibria in the Systems UF <sub>4</sub> -ThF <sub>4</sub> and
LiF-UF <sub>4</sub> -ThF <sub>4</sub> , ORNL-2719 (Aug. 17, 1959); J. Am. Ceram. Soc. <u>43</u> , 213 (1960).
$^{50}$ L. V. Jones et al., Phase Equilibria in the LiF-BeF <sub>2</sub> -UF <sub>4</sub> Ternary Fused Salt System, MLM-1080 (Aug. 24, 1959).
<sup>51</sup> R. E. Thoma (ed.), Phase Diagrams of Nuclear Reactor Materials, ORNL-2548, p 108-9 (Nov. 6, 1959). <sup>52</sup> R. E. Thoma, Results of Examinations of Fused Salt Mixtures by
Optical and X-Ray Diffraction Methods, ORNL CF-58-11-40, item 1925 (Nov.
14, 1958). <sup>53</sup> R. E. Thoma, <u>Results of X-Ray Diffraction Phase Analyses of Fused</u> <u>Salt Mixtures</u> , ORNL CF-58-2-59, items 1873 and 1894 (Feb. 18, 1958).
<sup>54</sup> R. E. Thoma, <u>Results of Examinations of Fused Salt Mixtures by</u> Optical and X-Ray Diffraction Methods, ORNL CF-59-10-18, items 2006, 2010 2036 2056 2061 and 2077 (opt 7, 1050)

Solid-state equilibrium is readily established if the solid mixture is annealed for a short time at temperatures near the solidus.



Fig. 7. The System LiF-BeF<sub>2</sub>-UF<sub>4</sub>.

Numerous investigations of the interactions of molten mixtures of LiF, BeF<sub>2</sub>, and UF<sub>4</sub> with other substances have been reported. The solu-



Fig. 8. The System LiF-BeF2-UF4.

Table	5.	Invariant	Equilibria	in	the	System	LiF-BeF2-UH	74*
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Composition of Liquid (mole %)			Tempera- ture	Type of	Solid Phases Present at
LiF	BeF <sub>2</sub>	UF4	(°C)	Equilibrium	Invariant Temperature
72	6	22	480	Peritectic (de- composition of 4LiF·UF <sub>4</sub> in the ternary system)	4LiF.UF4, LiF, and 7LiF.6UF4
69	23	8	426	Eutectic	LiF, 2LiF.BeF2, and 7LiF.6UF4
48	51.5	0.5	350	Eutectic	7LiF.6UF4, 2LiF.BeF2, and BeF2
45.5	54	0.5	381	Peritectic	LiF.4UF4, 7LiF.6UF4, and BeF2
29.5	70	0.5	483	Peritectic	UF <sub>4</sub> , LiF•4UF <sub>4</sub> , and $BeF_2$

\*R. E. Thoma (ed.), Phase Diagrams of Nuclear Reactor Materials, ORNL-2548, p 109 (Nov. 6, 1959).

Table 6. Phase Behavior of Selected LiF-BeF2-UF4 Compositions

Temperature (°C)	Phases Present
C-75: 67	/ LiF-2.5 UF <sub>4</sub> -30.5 BeF <sub>2</sub> (Mole %)
464-450	LiF and liquid
450-426	LiF, 2LiF.BeF2, and liquid
Below 426	LiF, 2LiF.BeF2, and 7LiF.6UF4
C-126:	53 LiF-l UF <sub>4</sub> -46 BeF <sub>2</sub> (Mole %)
400-350	2LiF.BeF2, 7LiF.6UF4, and liquid
350-280	2LiF.BeF2, 7LiF.6UF4, and BeF2
Below 280	$2LiF \cdot BeF_2$ , $7LiF \cdot 6UF_4$ , and $LiF \cdot BeF_2$
C-130:	62 LiF-1 UF <sub>4</sub> -37 BeF <sub>2</sub> (Mole %)
440-414	2LiF.BeF2 and liquid
414-381	2LiF.BeF2, 7LiF.6UF4, and liquid
381-280	2LiF.BeF2, 7LiF.6UF4, and BeF2
Below 280	2LiF·BeF <sub>2</sub> , 7LiF·6UF <sub>4</sub> , and LiF·BeF <sub>2</sub>
C-131:	60 LiF-4 UF <sub>4</sub> -36 BeF <sub>2</sub> (Mole %)
450-415	7LiF.6UF4 and liquid
415-381	7LiF.6UF4, 2LiF.BeF2, and liquid
381-280	7LiF.6UF4, 2LiF.BeF2, and BeF2
Below 280	7LiF.6UF <sub>4</sub> , 2LiF.BeF <sub>2</sub> , and LiF.BeF <sub>2</sub>
C-136:	70 LiF-20 UF <sub>4</sub> -10 BeF <sub>2</sub> (Mole %)
500-465	7LiF.6UF4 and liquid
465-426	7LiF.6UF4, LiF, and liquid
Below 426	7LiF.6UF4, LiF, and 2LiF.BeF2

bilities of  $PuF_3$ ,<sup>12</sup>  $CeF_3$ ,<sup>55</sup>  $LaF_3$ ,<sup>55</sup> and  $SmF_3$ ,<sup>55</sup> in LiF-BeF<sub>2</sub>-UF<sub>4</sub> solvents and the reactions of BeO<sup>56</sup> and steam<sup>57</sup> on these solvents have been investigated. The exchange of  $SmF_3$  (dissolved) and  $CeF_3$  (solid),<sup>58</sup> the exchange of Hf in HfF<sub>4</sub> and HfC,<sup>59</sup> and the effect of  $AlF_3$ ,<sup>58</sup> on the solubility of the rare-earth trifluorides in LiF-UF<sub>4</sub>-BeF<sub>2</sub> molten mixtures have been studied. In addition the effect of thermal cycling on segregation,<sup>60</sup> the effect of radiation on static corrosion of graphite and of INOR-8,<sup>61</sup> graphite permeation,<sup>62</sup> dehydration,<sup>63</sup> and purification,<sup>64</sup> have been reported for LiF-UF<sub>4</sub>-BeF<sub>2</sub> mixtures.

#### 3.8 The System LiF-BeF2-ThF4

The phase equilibria in the system  $\text{LiF-BeF}_2-\text{ThF}_4$  (Figs. 9-15) have been described in a recent report.<sup>20</sup> One aspect of the phase equilibria in this system which is of significance is the formation of a solid solution in which beryllium replaces both lithium and thorium in the  $3\text{LiF}\cdot\text{ThF}_4$  lattice. The single-phase composition area for this solid solution is limited as indicated in Table 7. This results in the formation of phases at the solidus whose compositions are not so diverse as those which would have been formed if the substitutional solid solution

<sup>55</sup>R. A. Strehlow et al., Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960, ORNL-2931, p 77. <sup>56</sup>J. H. Shaffer, G. M. Watson, and W. R. Grimes, Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960, ORNL-2931, p 84. <sup>57</sup>Ibid., p 87. <sup>58</sup>R. A. Strehlow et al., Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960, ORNL-2931, p 77-80. <sup>59</sup>J. H. Shaffer and G. M. Watson, Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960, ORNL-2931, p 83. <sup>60</sup>G. J. Nessle and J. Truitt, <u>Reactor Chem. Ann. Prog. Rep. Jan. 31</u>, 1960, ORNL-2931, p 17-19. <sup>61</sup>W. E. Browning and H. L. Hemphill, <u>Reactor Chem. Ann. Prog. Rep.</u> Jan. 31, 1960, ORNL-2931, p 74-75. <sup>62</sup>R. J. Sheil et al., Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960, ORNL-2931, p 69. <sup>63</sup>C. J. Barton et al., Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960, ORNL-2931, p 20. <sup>64</sup>J. E. Eorgan et al., Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960, ORNL-2931, p 64.



Fig. 9. The System LiF-BeF2-ThF4.

Table 7. Limits of Single-Phase 3LiF.ThF4 Solid Solution\*

Composition in	mole	%
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LiF	BeF <sub>2</sub>	ThF <sub>4</sub>	
75	0	25	
58	16	26	
59	20	21	

\*R. E. Thoma (ed.), <u>Phase Dia-</u> grams of <u>Nuclear Reactor Materials</u>, ORNL-2548, p 81 (Nov. 6, 1959). in  $3\text{LiF} \cdot \text{ThF}_4$  were not to occur. This is a way of saying that when such mixtures are used as reactor fuels, the segregation of the thorium-containing phase or phases from the LiF-BeF<sub>2</sub> solvent on cooling will be less than one would expect without a knowledge of the solid solution.

No ternary compounds are formed in the system. Conse-

quently, all the solid phases formed in the system, except for members of the  $3\text{LiF}\cdot\text{ThF}_4$  solid solution, are the components or binary compounds described above (Secs 3.1, 3.2, 3.3, and 3.4). The compositions and the temperatures of the six invariant points may be found in Table 8.



Fig. 10. The System LiF-BeF<sub>2</sub>-ThF<sub>4</sub>.

The equilibrium phase behavior which will occur in several selected  $LiF-BeF_2-ThF_4$  compositions is described in Table 9.

When mixtures of LiF-BeF<sub>2</sub>-ThF<sub>4</sub> are cooled slowly from the liquid state, equilibrium is rarely, if ever, achieved. In compositions C-127, C-133 (or C-111a), and BeLT-15, solids have been routinely observed in the cooled melts which are indicative of nonequilibrium cooling. $^{65,66}$ 

<sup>65</sup>R. E. Thoma, <u>Results of X-Ray Diffraction Phase Analyses of Fused</u> Salt Mixtures, ORNL CF-58-2-59, item 1854 (Feb. 18, 1958).

<sup>66</sup>R. E. Thoma, <u>Results of Examinations of Fused Salt Mixtures by</u> Optical and X-Ray Diffraction Methods, ORNL CF-59-10-18, item 2095 (Oct. 7, 1959).



Fig. 11. The System LiF-BeF2-ThF4.



Fig. 12. The System LiF-BeF<sub>2</sub>-ThF<sub>4</sub>: 550°C Isotherm.



Fig. 13. The System LiF-BeF<sub>2</sub>-ThF<sub>4</sub>: 497°C Isotherm.

LiF. 4ThF

LiF-2ThFa

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JLIF-ThF4 BeF2 BeF2



Solid-state equilibrium is readily established if the solid mixture is annealed for a short time at temperatures near the solidus.

The system pairs  $\text{LiF-BeF}_2-\text{ThF}_4$  and  $\text{LiF-BeF}_2-\text{UF}_4$  are very similar. In both, the primary phase fields of the  $\text{LiF-BeF}_2$  compounds occupy a small area, and the lowest liquidus temperatures are very near those in the system  $\text{LiF-BeF}_2$ . A rather low temperature region exists on the liquidus surfaces in the vicinity of 70 mole % LiF. The liquidus surfaces in the

	Composi	$\frac{\text{Composition of Liquid}}{\text{(mole \%)}}$ $\frac{\text{BeF}_2  \text{ThF}_4}{83}  2$ $64  2.5$ $51.5  1.5$		Invariant Temperature	Type of	Solids Present	
	LiF	BeF <sub>2</sub>	ThF <sub>4</sub>	(°C)	Invariant	at invariant Point	
	15	83	2	497 ± 4	Peritectic	ThF <sub>4</sub> , LiF·4ThF <sub>4</sub> , and $BeF_2$	
	33.5	64	2.5	455 ± 4	Peritectic	LiF•4ThF4, LiF•2ThF4, and BeF2	
	47	51.5	1.5	356 ± 6	Eutectic	2LiF•BeF <sub>2</sub> , LiF•2ThF <sub>4</sub> , and BeF <sub>2</sub>	
*	60.5	36.5	3	433 ± 5	Peritectic	LiF•2ThF4, 3LiF•ThF4ss, and 2LiF•BeF2	
	65.5	30.5	4	444 ± 4	Peritectic	LiF, 2LiF•BeF <sub>2</sub> , and 3LiF•ThF <sub>4</sub> ss	
	63	30.5	6.5	448 ± 5	Peritectic	3LiF•ThF4ss, 7LiF•6ThF4, and LiF•2ThF4	
	*R. E. T	homa (ed.),	Phase Diagra	ms of Nuclear React	or Materials, ORNL	-2548, p 80 (Nov. 6, 1959).	

Table 8. Invariant Equilibria in the System  ${\tt LiF-BeF_2-ThF_4*}$ 

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Temperature (°C)	Phases Present
C-127: 58	8 LiF-7 ThF <sub>4</sub> -35 BeF <sub>2</sub> (Mole %)
460-430	LiF·2ThF <sub>4</sub> and liquid
430-356	LiF.2ThF4, 2LiF.BeF2, and liquid
356-280	$LiF \cdot 2ThF_4$ , $2LiF \cdot BeF_2$ , and $BeF_2$
Below 280	$LiF \cdot 2ThF_4$ , $2LiF \cdot BeF_2$ , and $LiF \cdot BeF_2$
C-133: 71	LiF-13 ThF <sub>4</sub> -16 BeF <sub>2</sub> (Mole %)
500-470	3LiF.ThF4ss and liquid
470-444	$3LiF \cdot ThF_4ss$ , LiF, and liquid
Below 444	$3LiF \cdot ThF_4ss$ and $2LiF \cdot BeF_2$
BeLT-15:* 6	7.5 LiF-15 ThF <sub>4</sub> -17.5 BeF <sub>2</sub> (Mole %)
500-465	$3LiF \cdot ThF_4ss$ , $7LiF \cdot 6ThF_4$ , and liquid
465-440	$3LiF \cdot ThF_4ss$ and liquid
Below 440	$3LiF \cdot ThF_4ss$ and $2LiF \cdot BeF_2$
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Table 9. Phase Behavior of Selected LiF-BeF<sub>2</sub>-ThF<sub>4</sub> Compositions

\*R. E. Thoma, Crystallization Reactions in the Mixture LiF-BeF<sub>2</sub>-ThF<sub>4</sub> (67.5-17.5-15 Mole %), BeLT-15, ORNL CF-59-4-49 (Apr. 13, 1959).

system LiF-BeF<sub>2</sub>-ThF<sub>4</sub> tend to occur at somewhat higher temperatures than those in the system LiF-BeF<sub>2</sub>-UF<sub>4</sub>.

Several investigations of the interactions of molten mixtures of LiF, BeF<sub>2</sub>, and ThF<sub>4</sub> have been reported. The precipitation of ThO<sub>2</sub> from LiF-BeF<sub>2</sub>-ThF<sub>4</sub> mixtures by steam<sup>40</sup> has been studied. Attempts to remove barium from LiF-BeF<sub>2</sub>-ThF<sub>4</sub> mixtures by adding  $Cr_2O_3$  or BeO were unsuccessful, as were attempts to remove cerium by adding BeO or Al<sub>2</sub>O<sub>3</sub>.<sup>41</sup> The segregation effect of thermal cycling on LiF-BeF<sub>2</sub>-ThF<sub>4</sub> mixtures has been reported.<sup>60,63</sup>

#### 3.9 The System BeF<sub>2</sub>-ThF<sub>4</sub>-UF<sub>4</sub>

The great similarity of the binary systems  $BeF_2-UF_4$  and  $BeF_2-ThF_4$ (Sec 3.2) and the continuous solid solution between  $UF_4$  and  $ThF_4$  (Sec 3.6) indicate that the phase equilibria in the system  $BeF_2-ThF_4-UF_4^{67}$  are essentially predictable from the limiting systems. This has been confirmed experimentally (Fig. 16). The system is dominated by the primary phase



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Fig. 16. The System BeF<sub>2</sub>-UF<sub>4</sub>-ThF<sub>4</sub>.

area of the  $UF_4$ -Th $F_4$  solid solution. The only solid phases existing at equilibrium are  $BeF_2$  and the  $UF_4$ -Th $F_4$  solid solution. The properties of these solids are given in Secs 3.1 and 3.6 and in Appendixes A and B. The system possesses a single boundary path and no ternary invariant

<sup>67</sup>C. F. Weaver, R. E. Thoma, H. A. Friedman, and H. Insley, J. Am. Ceram. Soc., in press.

points. All mixtures with liquidus temperatures below  $550^{\circ}$ C contain more than 97 mole % BeF<sub>2</sub>.

# 3.10 The System LiF-UF<sub>4</sub>-ThF<sub>4</sub>

The system LiF-UF<sub>4</sub>-ThF<sub>4</sub><sup>49</sup> (Figs. 17 and 18) is characterized by extensive ternary solid solutions<sup>68</sup> which are shown in Figs. 19-22. The

 $^{68}$ The phrase "ternary solid solution" as used here implies that the solid solution composition lies within the system LiF-UF<sub>4</sub>-ThF<sub>4</sub>. Each of the solid solutions in this system, however, may be formed from mixtures of two end members and in this sense is a binary series.



#### Fig. 17. The System LiF-UF<sub>4</sub>-ThF<sub>4</sub>.



Fig. 18. The System  $LiF-UF_4-ThF_4$ .





equilibrium phase behavior of a ternary system involving solid solutions can be clearly and unambiguously described only by an extensive series of isothermal sections, fractionation paths in the primary phase areas, and tie lines in the subsolidus regions. Four isothermal sections which illustrate the invariant and the subsolidus phenomena are shown in Figs. 23-26. The fractionation paths for the primary phase areas 80 of the solutions may be found in Fig. 27. Tie lines for three of the subsolidus two-phase regions are shown in Fig. 28.

The temperatures and compositions of the three ternary invariant points are listed in Table 10. The compatibility triangles associated with these invariant points are shown in Fig. 29 and Table 10.





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Fig. 21. The System LiF-UF<sub>4</sub>-ThF<sub>4</sub>: 53.8 Mole % LiF Section.

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- (\*) LiF + 4LiF  $\cdot$  UF<sub>4</sub> + 7LiF  $\cdot$  6 ThF<sub>4</sub> 7LiF  $\cdot$  6 UF<sub>4</sub> ss
- (*j*) LiF + 7LiF  $\cdot$  6ThF<sub>4</sub> 7LiF  $\cdot$  6UF<sub>4</sub> ss
- (*i*)  $3 \text{LiF} \cdot \text{ThF}_4$  ss + 7 LiF  $\cdot 6 \text{ThF}_4$  7 LiF  $\cdot 6 \text{UF}_4$  ss + LiF
- (カ) 3LiF・ThF<sub>4</sub> ss
- (g)  $4\text{LiF} \cdot \text{UF}_4 + 7\text{LiF} \cdot 6\text{ThF}_4 7\text{LiF} \cdot 6\text{UF}_4$  ss + LIQUID
- (f)  $4LiF \cdot UF_4 + LIQUID$
- (e)  $4 \text{LiF} \cdot \text{UF}_4 + \text{LIQUID} + \text{LiF}$
- (d)  $LiF + 7LiF \cdot 6ThF_4 7LiF \cdot 6UF_4 ss + LIQUID$
- (c)  $LiF + 3LiF \cdot ThF_4$  ss + LIQUID
- (b) LiF+LIQUID
- (a) LIQUID + 3LiF · ThF4 ss

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Fig. 24. The System LiF-UF<sub>4</sub>-ThF<sub>4</sub>: 500°C Isothermal Section.

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Fig. 25. The System LiF-UF4-ThF4: 488°C Isothermal Section.

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 $\sum_{i=1}^{n}$ 

Fig. 26. The System LiF-UF<sub>4</sub>-ThF<sub>4</sub>: 450°C Isothermal Section.



Fig. 27. The System LiF-UF<sub>4</sub>-ThF<sub>4</sub>: Fractionation Paths.



Fig. 28. The System LiF-UF<sub>4</sub>-ThF<sub>4</sub>: Tie Lines.

Composition of Solid Phases Invariant Point Invariant Type in Equilibrium (mole %) Temperature of at the Invariant (°C) Equilibrium Temperature LiF ThF<sub>4</sub>  $UF_4$ 19 18 609 63 Peritectic  $LiF \cdot 4ThF_4 - LiF \cdot 4UF_4ss$ containing 28 mole % UF4,  $LiF \cdot 2Th(U)F_4ss$ containing 23 mole % UF4, 7LiF.6ThF4-7LiF.6UF4ss containing 23 mole % UF<sub>4</sub>. 500 72.5 20.5 Peritectic 7LiF.6ThF4-7LiF.6UF4ss containing 31 mole % UF<sub>4</sub>, 3LiF.Th(U)F4ss containing 15.5 mole % UF<sub>4</sub>, LiF 72 26.5 1.5 488 Eutectic 7LiF.6ThF4-7LiF.6UF4ss containing 42.5 mole % UF4, 4LiF•UF4, LiF

\*C. F. Weaver et al., Phase Equilibria in the Systems UF<sub>4</sub>-ThF<sub>4</sub> and LiF-UF<sub>4</sub>-ThF<sub>4</sub>, ORNL-2719 (Aug. 17, 1959); J. Am. Ceram. Soc. <u>43</u>, 213 (1960).

Table 10. Invariant Equilibria in the System LiF-UF4-ThF4\*

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Fig. 29. The System LiF-UF<sub>4</sub>-ThF<sub>4</sub>: Compatibility Triangles.

3.11 The System LiF-BeF<sub>2</sub>-UF<sub>4</sub>-TbF<sub>4</sub> (Selected Portions)

Detailed phase equilibrium studies for an entire quaternary system require such a vast amount of time and money that they are usually completed over a number of years if at all. The system  $\text{LiF-BeF}_2-\text{UF}_4-\text{ThF}_4$ is no exception in this respect, and consequently the experimental work was directed toward compositions which posses sufficiently low liquidus and viscosity values to be of project interest.

The similarities between the systems  $BeF_2$ -ThF<sub>4</sub> and  $BeF_2$ -UF<sub>4</sub>, the systems LiF-ThF<sub>4</sub> and LiF-UF<sub>4</sub>, and the systems LiF-BeF<sub>2</sub>-ThF<sub>4</sub> and LiF-BeF<sub>2</sub>-UF<sub>4</sub> have been discussed in Secs 3.2, 3.5, and 3.8 of this report. Within the systems UF<sub>4</sub>-ThF<sub>4</sub> and LiF-UF<sub>4</sub>-ThF<sub>4</sub> extensive solid solutions are formed between corresponding compounds. The existence of these similar systems and of solid solutions between analogous compounds leads to the hypothesis

that  $UF_4$  and  $ThF_4$  are very nearly interchangeable in the quaternary mixtures with respect to their liquidus values and that the phase relationships in the quaternary system will be very much like those in the ternary systems LiF-BeF2-ThF4 and LiF-BeF2-UF4. Four sections of constant mole per cent LiF and BeF<sub>2</sub> were studied experimentally as a means of partially verifying this hypothesis. These sections contain 70 LiF and 10 BeF<sub>2</sub>, 67.5 LiF and 17.5  $BeF_2$ , 70 LiF and 6  $BeF_2$ , and 65 LiF and 25  $BeF_2$  (mole %). The first two sections include the compositions C-136 and BeLT-15 (see Appendix C). The experimental results of these experiments may be found in Table 11. The liquidus values along the first three joins are nearly linear functions of the composition (Figs. 30-32). The deviation from linearity in the fourth join (Fig. 33) is in the direction of lower liquidus temperatures. The ThF4-containing end member has the maximum liquidus temperature for all the joins, while the  $UF_4$ -containing end member has the minimum liquidus temperature for three of the four joins. The solid solution  $7\text{LiF} \cdot 6(U, \text{Th})F_{4}$  is the primary phase for all the compositions on the joins listed above. The interchangeability of UF4 and ThF<sub>4</sub> implies that a breeder blanket selected from the quaternary system or its limiting systems will contain the maximum concentration of ThF4 for a given temperature only if no UF4 is present. In other words, if UF4 is added an approximately equal amount of ThF4 must be removed to maintain the same liquidus temperature.

Mixtures containing a maximum amount of ThF<sub>4</sub> for a given temperature are found in the system LiF-BeF<sub>2</sub>-ThF<sub>4</sub> (Figs. 9-11) up to 568°C. Above 568° the mixtures must contain no BeF<sub>2</sub>; thus they will be binary mixtures of LiF and ThF<sub>4</sub>.

The members of a second series contain a small total mole percentage of UF<sub>4</sub> and ThF<sub>4</sub> (Table 11). They represent the breeder fuels, such as C-134, BULT 4-0.5U, and BULT 4-1U. Compositions containing up to 5 mole % UF<sub>4</sub> + ThF<sub>4</sub> in the range 30-38 mole % BeF<sub>2</sub> have liquidus values close to those of the system LiF-BeF<sub>2</sub>. These compositions differ from the LiF-BeF<sub>2</sub> binary mixtures in that their liquidus values are slightly lower and solid solutions containing UF<sub>4</sub> and ThF<sub>4</sub> precipitate as primary or

Table 11. Include Gradient Quench Data for the System Dir-Der2-OF4-The		Table 11.	Thermal	Gradient	Quench	Data	for	the	System	LiF-BeF2-UF4-ThF
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Composition (mole %)				Temperature <sup>a</sup>	Phases <sup>b</sup> Above Temperature	Phases <sup>b</sup> Below Temperature	
LiF	BeF <sub>2</sub>	$\mathrm{UF}_4$	$\mathrm{ThF}_4$			·	
55	35	3	7	427 ± 3	L <sup>C</sup> and 7LiF.6(U,Th)F <sub>4</sub> ss	L, 7LiF·6(U,Th) $F_4$ ss, and 2LiF·Be $F_2$	
56	35	2	7	432 ± 3	L and $7LiF.6(U,Th)F_4ss$	L, 7LiF•6(U,Th)F <sub>4</sub> ss, and 2LiF•BeF <sub>2</sub>	
57	35	3	5	488 ± 3	L	L and LiF•2ThF <sub>4</sub> ss	
57	35	3	5	480 ± 3	L and LiF•2ThF <sub>4</sub> ss	L and $7LiF.6(U,Th)F_4ss$	
57	35	3	5	433 ± 3	L and 7LiF•6(U,Th)F <sub>4</sub> ss	L, 7LiF•6(U,Th)F <sub>4</sub> ss, and 2LiF•BeF <sub>2</sub>	
58	35	2	5	498 ± 3	L	L and LiF•2ThF4ss (15 mole % UF4)	
58	35	2	5	460 ± 2	L and LiF•2ThF <sub>4</sub> ss	L and 7LiF.6(U,Th)F4ss (ll mole % UF4)	
58	35	2	5	433 ± 3	L and $7LiF.6(U,Th)F_4ss$	L, 7LiF•6(U,Th)F <sub>4</sub> ss, and 2LiF•BeF <sub>2</sub>	
59	35	3	3	479 ± 2	L	L and 7LiF.6(U,Th)F4ss (22 mole % UF4)	
59	35	3.	3	434 ± 2	L and 7LiF•6(U,Th)F <sub>4</sub> ss	L, 7LiF•6(U,Th)F <sub>4</sub> ss, and 2LiF•BeF <sub>2</sub>	
60	35	2	3	449 ± 2	L	L and $7LiF.6(U,Th)F_4ss$	
60	35	2	· 3	440 ± 2	L and $7LiF.6(U,Th)F_4ss$	L, 7LiF·6(U,Th)F <sub>4</sub> ss, and $2LiF\cdotBeF_2$	
60	35	2	3	<b>~</b> 425	L, 7LiF•6(U,Th)F4ss, and 2LiF•BeF2	2LiF·BeF <sub>2</sub> and 7LiF·6(U,Th)F <sub>4</sub> ss (20 mole % UF <sub>4</sub> )	

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	Comp (m	osition ole %)		Temperature <sup>a</sup>	Phases <sup>b</sup> Above Temperature	Phases <sup>b</sup> Below Temperature
LiF	BeF <sub>2</sub>	UF4	ThÉ <sub>4</sub>	(°C)	· · ·	
60	36	3	l	449 ± 2	Ĺ	L and 7LiF.6(U,Th)F4ss
60	36	3	1	432 ± 2	L and 7LiF.6(U,Th)F4ss	L, $2LiF \cdot BeF_2$ , and $7LiF \cdot 6(U,Th)F_4$
60	37	2	l ·	434 ± 2	L	L and $7LiF \cdot 6(U,Th)F_4ss$
60	37	2	1	431 ± 2	L and 7LiF•6(U,Th)F4ss	L, 7LiF•6(U,Th)F <sub>4</sub> ss, and 2LiF•BeF <sub>2</sub>
60	38	1	l	, 442 ± 2	L	L and 2LiF•BeF2
60	38	1	l	433 ± 2	L and 2LiF•BeF <sub>2</sub>	L, 2LiF•BeF <sub>2</sub> , and 7LiF•6(U,Th)F <sub>4</sub> ss (20 mole % UF <sub>4</sub> )
61	36	2	l	437 ± 2	L	L and $2LiF \cdot BeF_2$
61	36	2	l	434 ± 2	L and 2LiF•BeF <sub>2</sub>	L, 2LiF•BeF <sub>2</sub> , and 7LiF•6(U,Th)F <sub>4</sub> ss (23 mole % UF <sub>4</sub> )
61	37.5	0.5	ì	439 ± 3	L .	L and 2LiF•BeF <sub>2</sub>
62	34	3	l	446 ± 2	L	L and 7LiF.6(U,Th)F4ss
62	,34	3	l: ·	443 ± 2	L and 7LiF•6(U,Th)F4ss	L, 7LiF•6(U,Th) $F_4$ ss, and 2LiF•Be $F_2$
62	36	1.	l	446 ± 2	L	L and 2LiF•BeF2
62	36	l'	1	438 ± 2	L and $2LiF \cdot BeF_2$	L, 2LiF·BeF <sub>2</sub> , and 7LiF·6(U,Th)F <sub>4</sub> ss
62	36	, <b>1</b>	1	~420	L, $2LiF \cdot BeF_2$ , and $7LiF \cdot 6(U,Th)F_2ss$	2LiF•BeF <sub>2</sub> and 7LiF•6(U,Th)F2ss

Composition (mole %)				Temperature <sup>a</sup>	Phases <sup>b</sup> Above Temperature	Phases <sup>b</sup> Below Temperature		
LiF	BeF <sub>2</sub>	UF4	ThF <sub>4</sub>	(-0)				
62	36.5	0.5	1	452 ± 2	L	L and 2LiF.BeF <sub>2</sub>		
62	36.5	0.5	l	448 ± 3	L and $2LiF \cdot BeF_2$	L, 2LiF·BeF <sub>2</sub> , and 7LiF·6(U,Th)F <sub>4</sub> ss		
62	36.5	0.5	l	<b>~</b> 433	L, 2LiF•BeF <sub>2</sub> , and 7LiF•6(U,Th)F <sub>4</sub> ss	2LiF·BeF <sub>2</sub> and 7LiF·6(U,Th)F <sub>4</sub> ss		
63	35	l	l	450 ± 3	L	L and 2LiF•BeF <sub>2</sub>		
63	35	ļ	l	438 ± 3	L and $2LiF \cdot BeF_2$	L, 2LiF·BeF <sub>2</sub> , and 7LiF·6(U,Th)F <sub>4</sub> ss		
63	35	l	l	416 ± 3	L, 2LiF·BeF <sub>2</sub> , and 7LiF·6(U,Th)F <sub>4</sub> ss	2LiF·BeF <sub>2</sub> and 7LiF·6(U,Th)F <sub>4</sub> ss		
63	35	2	l	442 ± 2	L	L and $2LiF \cdot BeF_2$		
63	35	2	1	438 ± 2	L and 2LiF•BeF <sub>2</sub>	L, 2LiF•BeF <sub>2</sub> , and 7LiF•6(U,Th)F <sub>4</sub> ss (23 mole % UF <sub>4</sub> )		
63	35.5	0.5	l	456 ± 2	L	L and $2LiF \cdot BeF_2$		
63	35.5	0.5	l	448 ± 3	L and $2LiF \cdot BeF_2$ .	L, 2LiF·BeF <sub>2</sub> , and 7LiF·6(U,Th)F <sub>4</sub> ss		
64	32	3	l	446 ± 2	L	L and $2LiF \cdot BeF_2$		
64	32	3	l	443 ± 2	L and $2LiF \cdot BeF_2$	L, 2LiF·BeF <sub>2</sub> , and 7LiF·6(U,Th)F <sub>4</sub> ss		
64	33	2 ·	1.	442 ± 2	L	L and 2LiF•BeF <sub>2</sub>		

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Table 11 (continued)

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Composition (mole %)				Temperature <sup>a</sup>	Phases <sup>b</sup> Above Temperature	Phases Below Temperature	
LiF	BeF <sub>2</sub>	UF4	ThF <sub>4</sub>			• . •	
64	33	2	1	440 ± 2	L and 2LiF.BeF2	L, 2LiF·BeF <sub>2</sub> , and 7LiF·6(U,Th)F <sub>4</sub> ss (22 mole % UF <sub>4</sub> )	
65	25	3	7	477 ± 2	L	L and $7LiF \cdot 6(U, Th)F_4ss$	
65	25	3	7	437 ± 2	L and 7LiF•6(U,Th) $F_4ss$	L, 7LiF•6(U,Th)F4ss, and 2LiF•BeF2	
65	25	5	5	447 ± 3	L .	L and 7LiF•6(U,Th)F4ss (22 mole % UF4)	
65	25		5	437 ± 3	L and 7LiF.6(U,Th) $F_4$ ss	L, 2LiF•BeF <sub>2</sub> , and 7LiF•6(U,Th)F <sub>4</sub> ss	
65	25	5	5	430 ± 3	L, 2LiF·BeF <sub>2</sub> , and 7LiF·6(U,Th)F <sub>4</sub> ss	7LiF•6(U,Th)F <sub>4</sub> ss and 2LiF•BeF <sub>2</sub>	
65 <sup>°</sup>	25	8	2	442 ± 3	L	L and $7LiF \cdot 6(U, Th)F_4ss$	
65	25	8	2	432 ± 2	L and 7LiF•6(U,Th)F <sub>4</sub> ss	L, 7LiF.6(U,Th)F4ss (36 mole % UF4), and 2LiF.BeF2	
65	· 25	8	2	424 ± 2	L, 7LiF•6(U,Th)F <sub>4</sub> ss, and 2LiF•BeF <sub>2</sub>	LiF, 7LiF.6(U,Th)F4ss, and 2LiF.BeF2	
65	30	l	4	448 ± 2	L	L, 2LiF•BeF <sub>2</sub> , and 3LiF•ThF <sub>4</sub> ss	
65	30	_ 1	4	423 ± 2	L, 2LiF.BeF <sub>2</sub> , and 3LiF.ThF <sub>4</sub> ss	L, 2LiF·BeF <sub>2</sub> , and 7LiF·6(U,Th)F <sub>4</sub> ss (9 mole % UF <sub>4</sub> )	
65	30.5	0.5	4	453 ± 1	L	L and 3LiF.ThF4ss	
65	30.5	0.5	. 4	448 ± 2	L and 3LiF.ThF4ss	L, 3LiF.ThF4ss, and 2LiF.BeF2	

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	Compo (me	osition ole %)		Temperature <sup>a</sup>	Phases b Above Temperature	Phases <sup>b</sup> Below Temperature	
LiF	BeF <sub>2</sub>	UF4	ThF <sub>4</sub>	(''')			
65	31	3	l	449 ± 2	L	L and 2LiF.BeF2	
65	31	3	1	443 ± 2	L and $2LiF \cdot BeF_2$	L, $2LiF \cdot BeF_2$ , and $7LiF \cdot 6(U,Th)F_4ss$	
65	33	l	l	465 ± 1	L	L and 2LiF·BeF <sub>2</sub>	
65	33	1	l	446 ± 2	L and 2LiF•BeF <sub>2</sub>	L, 2LiF.BeF <sub>2</sub> , and 7LiF.6(U,Th)F4ss (22 mole % UF4)	
55	33	l	l	408 ± 2	L, 2LiF•BeF <sub>2</sub> , and 7LiF•6(U,Th)F <sub>4</sub> ss	2LiF·BeF <sub>2</sub> and 7LiF·6(U,Th)F <sub>4</sub> ss	
56.4	24.9	5.4	3.3	446 ± 2	L	L and 7LiF•6(U,Th)F4ss (21 mole % UF4)	
67	18.5	0.5	14	499 ± 4	L	L and 3LiF.ThF4ss	
67.5	17.5	3	12	490 ± 3	L	L and 7LiF.6(U,Th)F4ss	
57.5	17.5	3	12	480 ± 3	L and 7LiF.6(U,Th)F4ss	L, 7LiF•6(U,Th)F4ss, and 3LiF•ThF4ss	
67.5	17.5	3	12	429 ± 2	L, 7LiF•6(U,Th)F4ss, and 3LiF•ThF4ss	L and $3LiF \cdot hF_4ss$	
67.5	17.5	. 6.	9	490 ± 3	L	L and $7LiF.6(U,Th)F_4ss$	
67.5	17.5	6	9	462 ± 3	L and 7LiF•6(U,Th)F4ss	L, 7LiF•6(U,Th)F4ss, and 3LiF•ThF4ss	
67.5	17.5	6	9	429 ± 2	L, 7LiF•6(U,Th)F4ss, and 3LiF•ThF4	L, 7LiF.6(U,Th)F4ss, and 2LiF.BeF2	

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Composition (mole %)		Temperature <sup>a</sup>	Phases <sup>b</sup> Above Temperature		Phases <sup>b</sup> Below Temperature		
LiF	BeF2	UF <sub>4</sub>	$ThF_4$	(())		• .	
67.5	17.5	9	6	484 ± 3	L ``		L and 7LiF.6(U,Th)F4ss
67.5	17.5	9	6	438 ± 3	L and	7LiF•6(U,Th)F <sub>4</sub> ss	L, 7LiF•6(U,Th)F <sub>4</sub> ss, and 2LiF•BeF <sub>2</sub>
67.5	17.5	. 12	3	484 ± 3	L		L and $7LiF.6(U,Th)F_4ss$
67.5	17.5	12	. 3	43 <u>3</u> ± 3	L and	7LiF•6(U,Th)F4ss	L, 7LiF.6(U,Th)F4ss, and 2LiF.BeF2
68	18.7	10.8	2.5	446 ± 2	L	· · · ·	L and 7LiF•6(U,Th)F4ss (34 mole % UF4)
69.7	12.4	16.2	1.7	461 ± 2	L		L, LiF, and 7LiF•6(U,Th)F4ss (38 mole % UF4)
70	6	6	18	540 ± 2	$\mathbf{L}$		L and 7LiF•6(U,Th) $F_4ss$
70	6	6	18	531 ± 3	L and	$7 \text{LiF-6}(U, \text{Th}) \text{F}_4 \text{ss}$	L, 7LiF•6(U,Th)F4ss, and 3LiF•ThF4ss
.70	6	12	12	516 ± 2	L		L and 7LiF•6(U,Th)F4ss (16 mole % UF4)
70	6	12	12	503 ± 2	L and	7LiF•6(U,Th)F4ss	L, 7LiF•6(U,Th)F4ss, and 3LiF•ThF4ss
70	6	18	6	494 ± 3	L <sup>.</sup>		L and 7LiF•6(U,Th)F4ss (30 mole % UF4)
70	6	18	6	476 ± 2	L and	7LiF•6(U,Th)F4ss	L, 7LiF•6(U,Th) $F_4$ ss, and LiF
70	6	24	0 <sup>d</sup>	480 ± 3	L		L and $7LiF \cdot 6UF_4$
70 ·	6	24	Od	462 ± 2	L and	7Lif•6UF4	L, 7LiF.6UF4, and LiF

Composition (mole %)		Temperature <sup>a</sup>	Phases <sup>b</sup> Above Temperature	Phases <sup>b</sup> Below Temperature		
LiF	BeF <sub>2</sub>	UF₄	$\mathrm{ThF}_4$			
70	10	5	15	512 ± 3	L	L and 7LiF.6(U,Th)F4ss (6 mole % UF4)
70	10	5	15	510 ± 3	L and 7LiF·6(U,Th)F4ss (6 mole % UF4)	L, 7LiF·6(U,Th)F <sub>4</sub> ss, and 3LiF·ThF <sub>4</sub> ss
70	10	5	15	485 ± 3	L, 7LiF•6(U,Th)F4ss, and 3LiF•ThF4ss	L and 3LiF.ThF4ss
70	10	10	10	493 ± 3	L	L and 7LiF.6(U,Th)F <sub>4</sub> ss
70	10	10	10	489 ± 3	L and 7LiF.6(U,Th)F4ss	L, 7LiF•6(U,Th)F4ss, and 3LiF•ThF4ss
70	10	10	10	455 ± 3	L, 7LiF•6(U,Th)F4ss, and 3LiF•ThF4ss	L, 7LiF•6(U,Th)F <sub>4</sub> ss, and LiF
70	10	15	5	475 ± 3	L	L and 7LiF•6(U,Th)F4ss (28 mole % UF4)
70	10	15	5	471 ± 3	L and 7LiF•6(U,Th)F4ss	L, 7LiF.6(U,Th)F4ss (28 mole % UF4), and LiF
71	16	l	12	513 ± 2	L	L and 3LiF.ThF4ss
71.4	6.2	21.6	0.8	483 ± 1	L	L and 7LiF•6(U,Th)F4ss (13 mole % UF4)
71.4	6.2	21.6	0.8	480 ± 2	L and 7LiF•6(U,Th) $F_4$ ss	L, LiF, and 7LiF.6(U,Th) $F_4$ ss

Table 11 (continued)

<sup>a</sup>The uncertainty indicates the temperature difference between the quenched samples.

<sup>b</sup>Only phases found in major quantity are given. Minor quantities of other phases resulting from lack of complete reaction between solids or from trace amounts of oxide impurities are not noted. Glasses or poorly formed crystals assumed to have been produced during rapid cooling of liquid were found in those samples for which the observed phase is indicated as "liquid."

<sup>C</sup>L = liquid.

<sup>d</sup>This ternary mixture is included here because its liquidus temperature, as measured at ORNL, differs somewhat from that found on the Mound Laboratory diagram for the system LiF-UF<sub>4</sub>-BeF<sub>2</sub> (Fig. 7). 47



Fig. 30. The Join LiF-BeF<sub>2</sub>-ThF<sub>4</sub> (70-10-20)-LiF-BeF<sub>2</sub>-UF<sub>4</sub> (70-10-20) in the Quaternary System LiF-BeF<sub>2</sub>-ThF<sub>4</sub>-UF<sub>4</sub>.







Fig. 31. The Join LiF-BeF<sub>2</sub>-ThF<sub>4</sub> (67.5-17.5-15)-LiF-BeF<sub>2</sub>-UF<sub>4</sub> (67.5-17.5-15) in the Quaternary System LiF-BeF<sub>2</sub>-UF<sub>4</sub>-ThF<sub>4</sub>.



Fig. 33. The Join LiF-BeF<sub>2</sub>-ThF<sub>4</sub> (65-25-10)-LiF-BeF<sub>2</sub>-UF<sub>4</sub> (65-25-10) in the Quaternary System LiF-BeF<sub>2</sub>-UF<sub>4</sub>-ThF<sub>4</sub>.

secondary phases. Liquidus values rise sharply as the  $UF_4$  +  $ThF_4$  concentration is increased beyond 5 mole %.

The compositions referred to in the ORNL literature by code comprise a third series, which overlaps the group above. Their equilibrium behavior is described in Table 11 and Appendix C.

Melts which have been cooled slowly, rather than annealed and quenched, frequently contain nonequilibrium combinations of stable phases,



metastable phases, and glass. Consequently the phase analysis of slowly cooled melts cannot be relied upon to yield subsolidus equilibrium data. Supercooling is also observed and so affects the thermal analysis that this technique for studying heterogeneous equilibria cannot be used for the system  $\text{LiF-UF}_4$ -ThF\_4-BeF\_2.

It has been suggested that the uranium concentration in a molten salt reactor might be increased by adding the eutectic mixture of LiF and UF<sub>4</sub>.<sup>69</sup> Consequently, phase relationships in the quaternary section between 73 LiF-27 UF<sub>4</sub> and 64.75 LiF-4.15 ThF<sub>4</sub>-31.1 BeF<sub>2</sub> have been investigated. This join contains the fuel mixture 65 LiF-30 BeF<sub>2</sub>-4 ThF<sub>4</sub>-1 UF<sub>4</sub> (BULT 4-1U), and all the compositions which may be produced by mixing 73 LiF-27 UF<sub>4</sub> and 64.75 LiF-4.15 ThF<sub>4</sub>-31.1 BeF<sub>2</sub>. The results of thermal gradient quenching experiments may be found in Table 11. The liquidus values are shown as a function of composition in Fig. 34.



Fig. 34. The Join LiF-UF<sub>4</sub> (73-27)-LiF-BeF<sub>2</sub>-ThF<sub>4</sub> (64.75-31.1-4.15) in the Quaternary System LiF-BeF<sub>2</sub>-UF<sub>4</sub>-ThF<sub>4</sub>.

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Throughout the investigated portions of the quaternary system, the compositions of the solid solutions precipitating as primary phases indicate that the U/Th ratio is less in the solid which first appears than it is in the liquid phase. However, the concentration of uranium in these precipitates is frequently much higher than in the liquid phase.

Quaternary mixtures such as 62 LiF-36.5  $BeF_2-0.5 UF_4-1 ThF_4$ (mole %) (C-134) are hygroscopic and are prone to hydrolyze.<sup>70</sup>

Purified samples of this material were exposed to water-saturated air at room temperature, vacuum-dried at 135°C, and melted under vacuum

<sup>69</sup>F. F. Blankenship, ORNL, personal communication. <sup>70</sup>MSR Quar. Prog. Rep. Oct. 31, 1959, ORNL-2890, p 63. (Fig. 35). The cooled melts contained appreciable amounts of  $UO_2$ , which was detected by polarized light microscopy.<sup>63,70</sup> These results indicate



Fig. 35. Hydration-Vacuum-Dehydration Cycle for LiF-BeF<sub>2</sub>-ThF<sub>4</sub>-UF<sub>4</sub> (62-36.5-1-0.5).

ORNL-2931, p 67.

that a simple drying operation cannot be used with such mixtures and that to prevent hydrolysis these reactor fuels must be protected from water vapor even at room temperature.

Several investigations of the interaction of molten mixtures of LiF,  $BeF_2$ ,  $UF_4$ , and  $ThF_4$ with other substances may be found in the ORNL literature.

The solubility of  $CeF_3^{71}$  in LiF-BeF<sub>2</sub>-UF<sub>4</sub>-ThF<sub>4</sub> liquids and the reactions of BeO<sup>72</sup> and steam on these solvents have been reported. The exchange of CeF<sub>3</sub> (dissolved

in a quaternary solvent) and  $LaF_3$  (solid) has been studied.<sup>58</sup> The segregation effect of thermal cycling,<sup>60</sup> graphite compatibility,<sup>62</sup> and the leaching of chromium from INOR-8<sup>73</sup> have been investigated.

#### 4. ACKNOWLEDGMENTS

It is a pleasure to acknowledge the assistance of G. M. Hebert, who prepared a number of the quenched samples. We are especially grateful to J. H. Burns, F. F. Blankenship, H. G. MacPherson, and J. E. Ricci for suggestions and advice concerning many phases of the investigation.

<sup>71</sup>R. A. Strehlow <u>et al.</u>, <u>Reactor Chem. Ann. Prog. Rep. Jan. 31</u>, 1960, ORNL-2931, p 79.
 <sup>72</sup>J. H. Shaffer, G. M. Watson, and W. R. Grimes, <u>Reactor Chem. Ann.</u> Prog. Rep. Jan. 31, 1960, ORNL-2931, p 86.
 <sup>73</sup>J. E. Eorgan <u>et al.</u>, <u>Reactor Chem. Ann. Prog. Rep. Jan. 31, 1960</u>,

#### Appendix A

#### OPTICAL AND CRYSTALLOGRAPHIC PROPERTIES

The optical and crystallographic properties of the compounds which occur in the system LiF-UF<sub>4</sub>-ThF<sub>4</sub>-BeF<sub>2</sub> are summarized in Tables A-1 and A-2 respectively. No ternary or quaternary compounds have been observed. The refractive indices of the LiF-UF<sub>4</sub>-ThF<sub>4</sub> and UF<sub>4</sub>-ThF<sub>4</sub> solid solutions may be found in Figs. A-1 through A-5.

Compound	Optical	Optic	Optic	Refractive	e Indices	Color
Compound	Character	2V	Sign	$\mathbb{N}_{\omega}$ or $\mathbb{N}_{\alpha}$	$\mathbb{N}_{\in} \stackrel{\text{or } \mathbb{N}_{\gamma}}{\gamma}$	0101
Lif <sup>a</sup>	Isotropic			1.3915		Colorless
BeF2 <sup>b</sup>	Uniaxial		+	1.325		Colorless
UF4 <sup>C</sup>	Biaxial	~60°	-	1.552	1.598	Green
ThF4 <sup>b</sup>	Biaxial	~60°	—	1.500	1.534	Colorless
2LiF•BeF2 <sup>b</sup>	Uniaxial		+	1.312	1.319	Colorless
LiF•BeF <sub>2</sub>	Biaxial	Large		1.35 (av	verage)	Colorless
$4 \text{LiF} \cdot \text{UF}_4^{b}$	Biaxial	~10°		1.560	1.472	Green
7LiF•6UF4 <sup>b</sup>	Uniaxial			1.554	1.551	Green
LiF.4UF4	Biaxial	~10°	_	1.584	1.600	Green
3LiF•ThF4 <sup>d,e</sup>	Biaxial	~10°	_	1.480	1.488	Colorless
$7 \text{LiF} \cdot 6 \text{ThF}_4^d$	Uniaxial		÷	1.502	1.508	Colorless
$LiF \cdot 2ThF_4^d$	Uniaxial		-	1.554	1.548	Colorless
LiF.4ThF4 <sup>d,e</sup>	Biaxial	~10°	_	1.528	1.538	Colorless

Table A-1. Optical Properties of the Components and Binary Compounds in the System LiF-UF<sub>4</sub>-ThF<sub>4</sub>-BeF<sub>2</sub>

<sup>a</sup>Am. Soc. Testing Materials, <u>X-Ray Diffraction Data Cards</u>, card No. 4-0857. <sup>b</sup>H. Insley <u>et al.</u>, <u>Optical Properties and X-Ray Diffraction Data for Some</u> Inorganic Fluoride and Chloride Compounds, ORNL-2192 (Oct. 23, 1956).

<sup>C</sup>W. W. Harris and R. A. Wolters, <u>Optical Properties of UF4</u>, MDDC-1662 (Nov. 5, 1947); USAEC, <u>Abstracts of Declassified Documents</u>, vol 2, p 103, Technical Information Div., Oak Ridge, Tenn., 1948.

<sup>d</sup>R. E. Thoma et al., J. Phys. Chem. <u>63</u>, 1266 (1959).

<sup>e</sup>This routinely observed biaxiality appears to be a function of strain, since the crystal type is tetragonal as determined by x-ray diffraction measurements (see Table A-2).

Compound	Crystal		Lattice 1	Parameters	Space Group	X-Ray		
Compound	System	$a_0$ (A) $b_0$ (A)		c <sub>0</sub> (A) β		Space Group	(g/cc)	
Lif <sup>a</sup>	Cubic (face- centered)	4.0270				0 <sup>5</sup> <sub>h</sub> -Fm3m	2.638	
BeF2 <sup>b</sup>	Hexagonal	4.72		5.18		$D_6^4 = C6_22$ , $D_6^5 = C6_42$		
$\mathrm{ThF_4}^{C}$	Monoclinic	13.1	11.01	8.6	126°	$C_{2h}^6 - C2/c$	5.71	
UF4 <sup>c,d</sup>	Monoclinic	12.82	10.74	8.41	126°10'	$C_{2h}^{6} - C2/c$	6.70	
$7 \text{LiF} \cdot 6 \text{UF}_4^e$	Tetragonal	10.48		5.98		$I4_1/a$		
$3 \text{LiF} \cdot \text{ThF}_4^{f}$	Tetragonal	6.206		6.470		P4/nmm or P4/n	5.143	
$7 \text{LiF} \cdot 6 \text{ThF}_4^{f}$	Tetragonal	15.10		6.60		$I4_1/a$	5.387	
$\text{LiF} \cdot 2\text{ThF}_4^{f}$	Tetragonal	11.307		6.399		Body-centered(?)		
$\text{LiF} \cdot 4\text{ThF}_4^{f}$	Tetragonal	12.984		11.46				
2LiF•BeF2 <sup>g</sup>	Hexagonal	13.23		8.87			,	

Table A-2.	Crystallographic	Properties	of the	Components	and	the	Binary	Compounds
	Which Occu	ir in the Sy	ystem L	iF-UF4-ThF4·	-BeF <sub>2</sub>	2		

<sup>a</sup>Am. Soc. Testing Materials, <u>X-Ray Diffraction Data Cards</u>, card No. 4-0857; H. E. Swanson and E. Tatge, J C Fel. Reports, NBS 1949.

<sup>b</sup>This is the  $\beta$ -quartz form of BeF<sub>2</sub> routinely observed in the systems described in this report. The  $\beta$ -quartz and three other forms of BeF<sub>2</sub> are described by A. V. Novoselova, Uspekhi Khim 27, 33 (1959).

<sup>C</sup>W. H. Zachariasen, Acta Cryst. 2, 388 (1949).

<sup>d</sup>Am. Soc. Testing Materials, X-Ray Diffraction Data Cards, card No. 8-428.

<sup>e</sup>L. A. Harris, <u>The Crystal Structures of 7:6 Type Compounds of Alkali Fluorides with Uranium</u> <u>Tetrafluoride</u>, ORNL CF-58-3-15 (Mar. 6, 1958).

<sup>f</sup>L. A. Harris, G. D. White, and R. E. Thoma, J. Phys. Chem. <u>63</u>, 1974 (1959).

<sup>g</sup>Am. Soc. Testing Materials, <u>X-Ray Diffraction Data Cards</u>, card No. 6-0557; E. Thilo and H. A. Lehmann, Z. anorg. Chem. 258, 332 (1949).

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Fig. A-1. Refractive Indices of the  $UF_4$ -ThF<sub>4</sub> Solid Solutions.

1.1

Fig. A-2. Refractive Indices of the LiF.4UF<sub>4</sub>-LiF.4ThF<sub>4</sub> Solid Solutions.



Fig. A-3. Refractive Indices of the  $LiF \cdot 2Th(U)F_4$  Solid Solutions.



Fig. A-4. Refractive Indices of the  $7LiF.6UF_4-7LiF.6ThF_4$  Solid Solutions.





Appen	dix	В
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۲.i F <sup>a</sup>			 የትም /	ThF, (continued)	
		l			
BeF <sub>2</sub>	b	d (A)	I/I1	d (A)	I/I1
d (A)	$I/I_1$	7.63	10	2.528	12
· • • • •	~~~	5.24	10	2.495	12
4.09	70	4.75	20	2.361	5
3.21	100	4.46	12	2.350	10
2.367	100	4.29	20	2.338	10
2.189	100	4.02	60	2.259	5
2.154	100	3.80	100	2.242	. 5
1.905	70	3.72	5	2,196	5
1.748	50	3.63	50	2.156	15
1.606	35	3.43	15	2,132	35
1.591	20	3.35	50	2.113	35
1,550	30	3.04	5	2.067	5
1.484	30	2.848	5	2.040	.20
1.320	30	2.796	5	2.023	20
1.233	15	2.747	15	1.985	35
1 208	בב ז ק י	2 723	エン . ち	1 965	15
1.200		2.125	· )	1.907	19
c		2.029	2	L.937	- TO
UF4				1.922	25

X-RAY DIFFRACTION DATA FOR THE SOLID PHASES OBSERVED IN THE QUATERNARY SYSTEM LiF-BeF<sub>2</sub>-UF<sub>4</sub>-ThF<sub>4</sub>

$ThF_4$ (continued)		3LiF• (metas	UF <sub>4</sub> table)	7LiF•6 (conti:	UF4 <sup>b</sup> nued)
d (A)	I/I1	d (A)	I/I1	d (A)	I/I1
1.881 1.859 1.771 1.737 1.683 1.666 1.640 1.612 1.588 1.575 1.520 1.484 1.455 1.431 1.404 1.373	10 5.5 10 10 20 10 10 10 5 10 20 5 20 10 5	4.98 4.80 4.41 4.34 3.98 3.91 3.60 3.40 3.14 3.07 2.84 2.771 2.529 2.169 2.083	20 15 100 100 15 8 80 10 25 50 80 30 35 15 75	3.33 3.15 3.07 2.99 2.771 2.707 2.542 2.350 2.286 2.264 2.184 2.097 2.060 2.047 1.993	90 70 10 95 30 30 25 13 25 13 10 30 30 30 75 25
/TiTe	ď, m	2.055	35 50	1.972	20 <u>4</u> 25
d (A)	I/I1	1.913 1.861	· 25 30	1.924 1.909	15 30
5.67 5.46 5.13 4.93 4.55 4.44	20 25 70 100 45 100	1.751 1.723 1.685 1.662 1.646 1.599	25 25 25 8 20 8	1.854 1.825 1.773 1.757 1.709 1.680 1.625	45 20 20 25 15 15 15
4.23	7 40	7LiF•6	UF4	1.579	25 8
3.55 3.03 2.89	30 50 25	d (A)	I/I <sub>1</sub>	LiF·4	JF4 <sup>b</sup>
2.000 2.747 2.468 2.398 2.221 2.167 2.074 2.025 1.872 1.836	50 50 20 40 75 20 20 25	5.97 5.82 5.24 5.15 4.65 4.37 3.95 3.85 3.68 3.49	20 15 90 10 13 55 13 20 75	7.02 6.33 6.07 5.73 4.98 4.70 4.25 3.88	8 12 5 25 8 25 90 20

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Appendix B (continued)

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Appendix B (continued)

$\text{LiF.4UF}_4^b$ (continued)	3LiF•1 (conti	hF4 <sup>d</sup> nued)	LiF•25	ſhF4 <sup>d</sup>
d (A) I/I1	d (A)	I/I1	d (A)	I/I1
$\begin{array}{cccc} 3.78 & 100 \\ 3.52 & 90 \\ 3.16 & 8 \\ 3.13 & 8 \\ 3.06 & 12 \\ 2.84 & 40 \\ \end{array}$	1.701 1.661 1.618 1.547 1.520	35 10 10 35 35	7.97 6.37 3.96 3.57 3.25 3.21 2.97	5 10 100 65 5 5 20
2.771 55 2.542 8	7LiF•6	ThF4 <sup>d</sup>	2.822 2.675	25 . 7
2.350 10 2.310 10	d (A)	I/I1	2.528 2.388	10 5
2.220       0         2.000       10         2.088       35         2.016       60         1.991       50         1.888       20         1.819       8         1.767       25	6.07 5.91 5.36 5.25 4.95 4.85 4.75	15 20 90 15 30 20 100	2.123 2.053 2.001 1.787 1.701 1.689 1.603 1.519	85 30 65 7 10 5 5 5
3LiF.ThF4 <sup>d</sup>	3.92	15	LiF•47	ChF4
d (A) I/I <sub>l</sub>	3.55	15 65 10	d (A)	I/I1
	3.39 3.29 3.03 2.814 2.747 2.578 2.430 2.392 2.302 2.137 2.018 2.001 1.892 1.859 1.804 1.653 1.600	70 60 100 25 25 20 10 10 20 20 5 15 55 15 15 15 15 15 20 20	8.34 7.76 6.51 5.80 4.62 4.33 3.88 3.60 3.25 2.92 2.822 2.603 2.398 2.137 2.053 2.040 2.018 2.005	3 3 5 25 5 70 100 60 10 25 25 10 10 25 35 10 10 20 30

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Appendix B	(continued)
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$\text{LiF.4ThF}_{4}^{d}$ (continued)		LiF·B	eF2 <sup>f</sup>	$LiF \cdot BeF_2^{f}$ (continued)	
(A) b	I/I1	d (kX)	I/I1	d (kX)	I/I1
1.937 1.820 1.778 1.725 1.719 1.666 1.605 1.595 1.563	20 20 3 5 5 5 5 5 5 5	4.353 3.180 3.084 2.926 2.836 2.780 2.739 2.455 2.259 2.201	20 50 20 5 50 10 40 50 100	2.040 1.829 1.691 1.558 1.488 1.439 1.324 1.303 1.244 1.233	20 10 5 2 10 1 2
2LiF•BeF2 <sup>e</sup>		2.074	80	1.216	2

<sup>a</sup>Am. Soc. Testing Materials, <u>X-Ray Diffraction Data Cards</u>, card No. 4-0857.

<sup>b</sup>H. Insley et al., <u>Optical Properties and X-Ray Diffraction Data for</u> <u>Some Inorganic Fluoride and Chloride Compounds</u>, ORNL-2192 (Oct. 23, 1956).

<sup>C</sup>Am. Soc. Testing Materials, <u>X-Ray Diffraction Data Cards</u>, card No. 8-428.

<sup>d</sup>R. E. Thoma et al., J. Phys. Chem. <u>63</u>, 1266 (1959).

<sup>e</sup>Am. Soc. Testing Materials, <u>X-Ray Diffraction Data Cards</u>, card No. 6-0557.

<sup>f</sup>E. Thilo and H. A. Lehmann, Z. anorg. Chem. 258, 332-55 (1949).

Code	Composition (mole %)				Liquidus Temperature	Primary Phase	
· · ·	LiF	BeF <sub>2</sub>	UF4	ThF <sub>4</sub>	(°C)	or Phases	
C-9	•	100			548	BeF <sub>2</sub>	
C-10	100				845	LiF	
C-74	69	31			530	LiF	
C-75	67	30.5	2.5		464	LiF	
C-111	71.	16	l	12	505	$3LiF \cdot ThF_4ss$	
C-112	50	50	·		370	2LiF•BeF2	
C-126	53	46	l		400	2LiF•BeF <sub>2</sub>	
C-127	58	35		7	460	LiF•2ThF4	
C-128	71			29	568*	3LiF•ThF4 and 7LiF•6ThF4	
C-130	62	37	l		440	2LiF•BeF <sub>2</sub>	
C-131	60	36	4		450	$7 \text{LiF} \cdot 6 \text{UF}_4$	
C-132	57	43			420	2LiF•BeF <sub>2</sub>	
C-133 (111-a)	71	16		13	505	$3LiF \cdot ThF_4ss$	
C-134	62	36.5	0.5	l	445	2LiF•BeF <sub>2</sub>	
C-136	70	10	20		500	$7LiF \cdot 6UF_4$	
BeLT-15	67	18		15	500	$7LiF \cdot 6ThF_4$ and $3LiF \cdot ThF_4ss$	
BULT 4-0.5U	65	30.5	0.5	4	453	$3LiF \cdot ThF_4ss$	
BULT 4-1U	, 65	30	1	4.	448	2LiF•BeF <sub>2</sub> and 3LiF•ThF <sub>4</sub> ss	
BULT 14-0.5U	67	18.5	0.5	14	500	7LiF•6(Th,U)F4ss and 3LiF•ThF4ss	
FULi 73	73		27		490*	$4LiF \cdot UF_4$ and $7LiF \cdot 6UF_4$	

LIQUIDUS TEMPERATURES AND PRIMARY PHASES FOR SPECIFIC COMPOSITIONS

Appendix C

\*The solidus and liquidus coincide, since these are eutectic compo-sitions.

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